Graphene-Enhanced Brillouin Optomechanical Microresonator for Ultrasensitive Gas Detection

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Supporting Information

ABSTRACT: Chemical sensing is one of the most important applications of nanoscience, whose ultimate aim is to seek higher sensitivity. In recent years, graphene with intriguing quantum properties has spurred dramatic advances ranging from materials science to optoelectronics and mechanics, showing its potential to realize individual molecule solid-state sensors. However, for optical sensing the single atom thickness of graphene greatly limits the light-graphene interactions, bottlenecking their performances. Here we demonstrate a novel approach based on the forward phase-matched Brillouin optomechanics in a graphene inner-deposited high Q (>2 × 10^6) microfluidic resonator, expanding the “electron−photon” interaction in conventional graphene optical devices to the “electron−phonon−photon” process. The molecular adsorption induced surface elastic modulation in graphene enables the Brillouin optomechanical modes (mechanical Q ≈ 43,670) extremely sensitive (200 kHz/ppm) in ammonia gas detection, achieving a noise equivalent detection limit down to 1 ppb and an unprecedented dynamic range over five orders-of-magnitude with fast response. This work provides a new platform for the researches of graphene-based optomechanics, nanophotonics, and optical sensing.

KEYWORDS: Graphene, Brillouin optomechnics, whispering gallery mode microresonator, fiber interrogated optics, ultrasensitive gas detection

Since discovered in 2004,1 graphene has brought unprecedented breakthroughs across the domains of optoelectronics, mechanics, and thermal transport, driven by its quasiparticle Dirac Fermions obeying a linear dispersion in the individual quanta level.2 Accordingly, graphene shows the unique potential to realize broadband optoelectronic modulators3−5, ultrasfast light sources/detectors,6,7 optomechanical devices,8−11 and highly sensitive bio and chemical sensors.12−14 Significantly, graphene enables gas detection with single molecule sensitivity on solid-state gas detectors, as gas adsorption on graphene changes the local carrier concentration.15−17 In contrast, limited by the graphene−light interaction efficiency, most graphene-based optical gas sensors have a maximum sensitivity of sub part per million (ppm),18 showing no significant advantages over existing techniques. To breakthrough this limit and realize a graphene-based optical sensor with individual molecule sensitivity, both the sensing mechanism and the associated technique need to be further explored.

Here we report a graphene based optomechanical microresonator and demonstrate its potential for ultrasensitive gas detection. A layer of nanometer-thick reduced graphene oxide (rGO) film is uniformly incorporated in a whispering gallery mode (WGM) bottle-shaped cavity with optical Q-factor >2 × 10^6, enhancing the forward phase-matched stimulated Brillouin scattering (F-SBS) resonance with a mechanical Q-factor ≈43 670 for a selected resonant mode at 262 MHz. In previous reports, optomechanics in a WGM cavity has shown exceptionally ultralow dissipation and ultrahigh phase correlation19 with great potential in optofluidics20 and light storage.21 However, to apply the F-SBS to detect gas is still elusive. In this

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work, the in-cavity deposited rGO enhances the high order WGM modes and modulates the F-SBS based optomechanical resonances based on gas molecule adsorption, expanding the “electron–photon” interaction in conventional graphene-based photonic sensors to the “electron–phonon–photon” interaction. Measured via RF spectroscopy with single Hz resolution, the fiber-coupled compact all-optical sensor based on the graphene enhanced Brillouin optomechanical microresonance approaches a detection limit down to 1 part per billion (ppb) and a wide dynamic range over 5 orders of magnitude.
magnitude (1 ppb to 370 ppm) for ammonia gas, an important chemical compound in industrial, environmental, and safety monitoring.

Figure 1a demonstrates the schematic design of the graphene enhanced Brillouin microresonator (GBMR). A microscale bottle-shaped capillary serves as both the optomechanical cavity and the gas fluidic channel. A tapered fiber with diameter of ≈1 μm is applied to launch and collect optical modes from the resonator along the x-axis, while gas molecules are injected into the cell along the y-axis. By using the fiber-splicer based arc discharge method, we fabricated the bottle-shaped microresonator (BMR) from a silica capillary (inner diameter 83 μm, outer diameter 100 μm), the diameter of the bottle-shaped section is 119 μm with silica wall thickness 8 μm. A layer of rGO film is deposited on the inner wall of the BMR via aqueous reduction technique. The thickness of the rGO film is estimated to be 3–5 nm.24,25 Figure 1b shows the micrographs of the GBMR and Raman spectrum of the rGO deposition. Driven by 1550 nm laser excitation, insertion loss of the GBMR is ≈5 dB. The inset of the Raman spectrum shows a scanning electron micrograph of the thin rGO film, verifying its uniformity. Fabrication process is detailed in Supplementary Figure S3.

The sensing mechanism of the GBMR for gas detection is shown in Figure 1c. Different from single-mode fibers predominantly supporting 11 GHz backward SBS, WGM cavities allow F-SBS ranging from tens of megahertz to tens of gigahertz, when the optical modes and the acoustic mode satisfy the energy and momentum conservation, that is, \( f_p = f_s + \frac{n_k}{c} k_M \), \( k_M = k_s + k_k \). Here subscript p, s, and M denote the pump mode, the Stokes mode, and the acoustic mechanical resonance mode, respectively. Referring to acoustic dispersion \( f_{ac} = \frac{\nu_a k_M}{c} \) and optical dispersion \( k_{opt} = 2\pi f_{opt} / \lambda \), we can describe the phase-matching condition as

\[
\frac{f_p}{f_s} = \frac{c - 2\nu_a n_p / c}{c - 2\nu_a n_s}.
\]

where \( \nu_a \) is the effective in-cavity acoustic velocity, and \( n_p \) and \( n_s \) are the effective refractive indexes of the pump mode and the Stokes mode, respectively (\( n_p > n_s \)). \( c \) is the light velocity in vacuum. To satisfy eq 1, \( n_p \) should be smaller than \( n_M \), meaning that the pump mode and the Stokes mode should be in different orders. For a phase-matched F-SBS in the optomechanical cavity, once the pump frequency is fixed the resonant Stokes frequency is determined by \( \nu_a \), which is proportional to the square of the elastic modulus in the microresonator. The gas molecules adsorbed on the surface of graphene, causing local lattice strain to change,22 which subsequently modifies the value of \( \nu_a \) and hence the phase matching condition. Theoretical analysis is in Supplementary Section S1. As a result, the number of gas molecules on the rGO surface, which correlates with the gas concentration in the sensing cell, can be accurately detected using an RF analyzer that monitors the optical heterodyne beat collected from the tapered fiber.

Figure 2a plots the transmissions of the BMR versus a GBMR, in range of 1530 to 1570 nm. Determined by its geometry, the GBMR designed for tunable F-SBS excitation exhibits many high-order mode resonances. Moreover, due to the rGO film (a high index material) deposition, high-order modes in the GBMR are dramatically enhanced compared to the BMR. Such an optical enhancement is directly reflected in the free spectrum ranges (FSRs).26 In the BMR, the FSR of the fundamental mode is ≈4.4 nm, while the FSR of the fundamental mode in the GBMR is ≈5.7 nm, also suggesting the effective index of the GBMR is smaller than the BMR.

Figure 2b expands on the transmission and compares the resonant dips of the BMR and the GBMR (here their extinction ratios are normalized, the resonances are selected around 1552 nm: \( \Lambda_{BMR} = 1551.75 \) nm, \( \Lambda_{GBMR} = 1552.53 \) nm). The optical Q-factor of the fundamental (TM0) mode of the BMR here is \( \approx 8 \times 10^6 \), which is typical for a silica bottle-shaped cavity. The WGM does not have much electrical field on the inner surface,
so the rGO absorption induced Q-factor reduction is relatively small, maintaining its maximum loaded Q-factor $\approx 2 \times 10^6$ (intrinsic $Q \approx 2.25 \times 10^6$), for the fundamental mode. High-order resonant modes close to the fundamental mode are observed, where the mode-to-mode spectral distance ranges from several megahertz to hundreds of megahertz. We note that the Q-factors of different resonances are varied; typically, a resonance of higher order mode or stronger scattering has lower Q-factor. More details are shown in Supplementary Figure S4. Figure 2c shows the “round trip transmission–resonance depth” correlation. In our measurements, the fiber-to-cavity coupling rate is $\approx 4\%$ and the BMR cavity is in the overcoupled regime. Because of the graphene induced loss, the GBMR is closer to the critical coupling point.

By tuning pump wavelength to 1552.717 nm (power launched in the GBMR $P_p = 400 \mu W$, higher than the F-SBS threshold $P_{th} \approx 250 \mu W$), we excite an optomechanical mode with $f_M = 262$ MHz in the GBMR (in air, room temperature). Figure 2d demonstrates the pump and the Stokes line in a high-resolution optical spectrum analyzer (OSA). The generated Stokes line is located at 1552.719 nm, an $\approx 2$ pm offset from the pump. In addition, there is no anti-Stokes line or cascaded harmonics, verifying that only F-SBS contributes in this nonlinear process. With finite element computation, we also illustrate the simulated mode distributions of the pump and Stokes mode in the insets with the longitudinal mode order at the pump frequency $N_p = 344$, and $N_s = 320$. In this case, we also have a longitudinal mode order of the acoustic mechanical resonance $N_M = 24$. Correspondingly, Figure 2e shows the pump-Stokes beat note in a RF spectrum analyzer. The location of the mechanical resonance is at 262 MHz and its signal-to-noise ratio is higher than 30 dB. The insets of Figure 2e illustrate the simulated mechanical mode distribution in the cavity and the measured mechanical line width of the beat note $\Delta f_M$ of $\approx 6$ kHz, estimating its mechanical $Q \approx 43,670$. Such a narrow line width is determined by both the phase matching of the F-SBS and the lasing excitation process.

Following the observations of the Brillouin and acoustic mechanical scattering, an ammonia gas ($\text{NH}_3$) sample is introduced into the capillary gas cell by using a microinjection system with concentration ranging from 1 to 10 ppm and with a fixed flow rate of 1 nL/min. The volume of the GBMR for gas filling is $\approx 0.7$ nL. That means under typical atmospheric pressure and room temperature 1 ppm of $\text{NH}_3$ gas in this GBMR has $\approx 1.84 \times 10^7 \text{NH}_3$ molecules. Experimental setup
and gas sample preparation are shown in Supplementary Figure S5 and Figure S6.

Figure 3a maps the measured RF spectra in NH₃ detection. When the GBMR cell filled with air, the beat note peak is located at 262.0 MHz originally. Perturbed by NH₃ injection with concentrations of 1, 2, 5, and 10 ppm, the beat note peak shifts to 261.8, 261.6, 261.1, and 260.4 MHz, respectively. It reflects that the mechanical resonance responds effectively to the gas molecule adsorption on the rGO film. We also note that such a spectral shift does not change the mode-to-mode phase matching and the mechanical mode order is kept at 24. Hence, during the gas sensing process the mechanical Q remains almost the same. Figure 3b demonstrates the NH₃ concentration versus Δf correlation of the GBMR (blue circles), where Δf is the RF spectral shift. By injecting NH₃ with the concentration ranging from 0 to 20 ppm, |Δf| increases by 2.75 MHz correspondingly. Because of small volume of the GBMR, note, uncertainty of the mechanical mode, and the phase noise Maximum sampling resolution of our RF analyzer is 1 Hz, accurately, it is worth characterizing its maximum resolution.

Figure 3c illustrates the dynamic range of the GBMR. It is known that graphene-based gas sensors tend to be saturated when gas concentration is too high, determined by the effective surface area of the graphene. Once all surface sites of graphene are filled, further spectral shift would be too small to detect. As illustrated in Figure 4c, the correlation of sensitivity decreases exponentially with concentration. When the NH₃ concentration is higher than 450 ppm, the sensitivity is lower than 200 Hz/ppm, as the blue dots show. Meanwhile, considering the influence of the frequency uncertainty, we estimate that once the NH₃ concentration is higher than 370 ppm, the RF shift cannot be detected stably. That means to detect NH₃ gas with sub-ppm sensitivity, the dynamic range is up to 370 ppm, comparable to prior graphene-based gas sensors with detection range from tens of ppm to thousands of ppm. Consequently, for our ppb detection limit our dynamic range is over 5 orders of magnitude.

In the above demonstrations, we mostly focus on the selected mechanical mode with order Nₘ = 24 and fₘ = 262 MHz. Actually, in the GBMR there are multiple excitable mechanical modes satisfying both the phase-matching condition of the F-SBS and the FSRs of the resonator. By carefully tuning the pump frequency, we also generated other mechanical modes, such as modes with fₛ = 103 MHz (Nₛ = 10) and fₛ = 775 MHz (Nₛ = 57). Referring to eq 1, the sensitivity (S) of the GBMR is proportional to its momentum

\[ S = \frac{\partial f}{\partial x} = \frac{2\pi n_p - 2\pi n_s}{(\varepsilon - 2\pi n_p)\nu_p} \frac{\partial \nu_p}{\partial x} \]

Here x is the gas concentration, νₚ is the acoustic velocity of an acoustic mode, and each generated mechanical mode corresponds to a specific nₛ. According to eq 2, for a fixed nₛ and fₚ, a smaller nₛ brings higher sensitivity. It indicates that a higher-order mode is helpful for the sensitivity enhancement. On the other hand, S ∝ fₛ and this means for a pair of specific mode-to-mode phase matching a higher frequency pump can also achieve a higher sensitivity. Figure 4d,e illustrates several measured sensitivities, by using different optomechanical modes, which are generated by tuning fₛ. Besides the mechanical mode with resonant frequency 262 MHz, when tuning fₛ to 190.5, 192.1, 192.6, and 194.8 THz, mechanical modes with fₛ ≈ 103, 76, 297, and 775 MHz are observed. In gas sensing, they have varied sensitivities, as shown in Figure 4e. Among them, our selected 262 MHz mode has the highest sensitivity. In practice, the mechanical modes also have different resonance Q-factor, noise, and surface deformation, which would influence the sensing dynamics as well. Hence, for the gas detection by using a GBMR photon–phonon matching condition could be further optimized. Benefiting from its optical measuring method similar to fiber Bragg gratings (FBGs), in applications the resonant modes are easy to characterize with the potential for networking for distributed sensing in the future.

In the last one, based on the 262 MHz mode, we also compare the maximum sensitivity when the GBMR sensor detecting varied gas molecules, as Figure 4f demonstrates. Determined by the adsorption nature of graphene material, the GBMR shows it highly selective to polar molecules, that is, ammonia (≈200 kHz/ppm), acetone (≈160 kHz/ppm), water vapor (≈120 kHz/ppm), and ethanol (≈110 kHz/ppm), whereas it has a much lower sensitivity to nonpolar molecules, that is, p-xylene (≈20 kHz/ppm, due to condensation), and...
hydrogen (≤5 kHz/ppm). We also note that the detection recovery of a high boiling point gas like acetone, ethanol, and p-xylene takes a much longer time (up to minutes), hence this sensor is most appropriate to perform as an ammonia gas detector. This property is also helpful for broadening its future potential in applications like gas chromatography.17

In summary, leveraging unique properties of the reduced graphene oxide nanosheet, we build a bridge between Brillouin optomechanics and gas molecular adsorptions. In the graphene-enhanced Brillouin optomechanical microresonator demonstrated, we expand electron-photon interaction in conventional graphene based optical sensors to electron-photon interaction, realizing a new platform for ultrasensitive and fast ammonia gas sensing with a noise equivalent limit down to 1 ppb and a wide dynamic range over five orders-of-magnitude. Moreover, such a graphene inner-coated high-Q WGM resonator also paves the way for designing new graphene-based optical cavities, which have wide potential in applications like plasmonics,30 optofluidics,31 and optomechanical manipulations.32

■ ASSOCIATED CONTENT

Supporting Information
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Detailed information on the theoretical analysis, fabrication of the graphene inner-deposited microresonator, measurement of optical Q-factors, experimental setup, and preparation of the gas samples. Measured results of NH3 detection without RGO film and instability of the GBMR (PDF)

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Notes
The authors declare no competing financial interest.

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■ REFERENCES


Supplementary Information for

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The supplementary materials consist of:

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### S1. Theoretical analysis

**S1.1. Forward stimulated Brillouin scattering in WGM cavities**

In the WGM cavity supporting both surface acoustic modes and high density optical modes, phase matching condition of the forward stimulated Brillouin scattering (F-SBS) could be satisfied in different modes [S1], Stokes line could be generated from the pump, obeying:

\[ f_p = f_s + f_M \]  \hspace{1cm} (S1)
\[ \vec{k}_p = \vec{k}_s + \vec{k}_M \]  \hspace{1cm} (S2)

In the cavity, the generated acoustic surface modes and the optical modes have the same propagation direction approximately. Referring to the optical dispersion and the acoustic dispersion, Eq. (S2) could be transferred as

\[ \frac{f_M}{v_A} = \frac{2\pi f_p n_p}{c} - \frac{2\pi f_s n_s}{c} \]  \hspace{1cm} (S3)

Here \( v_A \) is the acoustic velocity, \( c = 3 \times 10^8 \text{ m/s} \) is the light velocity in vacuum, \( n_p \) and \( n_s \) is the effective index of the pump mode and the generated Stokes mode. Considering Eq. (S1), we can get the relationship of the \( f_p \) and the \( f_s \):

\[ f_s = \frac{c - 2\pi v_A n_p}{c - 2\pi v_A n_s} f_p \]  \hspace{1cm} (S4)

For a WGM resonator, it can support several transverse modes, which has varied effective indexes and FSRs -- any of them can be marked as \( TM_{XY,N} \). Here subscript \( X, Y, \) and \( Z \) shows the order of the transverse modes (determined by the geometry) and the longitude mode (determined by the optical frequency), respectively. By using finite element method and commercial software COMSOL MULTIPHYSICS 4.3, Figure S1a to 1c simulate 3 examples of the WGM modes in our silica bottle-shaped cavity (diameter 118 µm and wall thickness 8 µm, index of the silica 1.454 at 1550 nm). In the resonator, to accumulate enough energy higher than the nonlinear threshold and the detection threshold, both the pump and the generated Stokes line of the F-SBS should be located at high \( Q \) resonant frequencies, and the transverse modes of them are different. Transverse mode order of \( f_s \) is higher than that of \( f_p \).
Fig. S1. Simulated electric field distributions (sectional view). a, TM$_{01.347}$, ($\lambda = 1551.9$ nm), b, TM$_{11.342}$, ($\lambda = 1561.0$ nm), c, TM$_{02.346}$, ($\lambda = 1544.2$ nm). In this figure the bar shows 10 µm.

Commonly, intensity of the phonon excitation is proportional to the pump power $P_p$, and the effective transmission length $L_{\text{eff}}$, as

$$I_M \propto \exp\left[ g_B P_p L_{\text{eff}} / A_{\text{eff}} \right]$$

(S5)

Here $g_B$ is the Brillouin gain coefficient, $A_{\text{eff}}$ is the effective transverse mode field distribution. In the resonator, $L_{\text{eff}}$ is determined by the $Q$ factor, i.e. a higher $Q$ brings a larger $L_{\text{eff}}$. For instance, in our GBMR with $Q \approx 2 \times 10^6$, $L_{\text{eff}}$ of the TM$_{01}$ mode could be as long as tens of kilometers, which is helpful reducing F-SBS threshold lower than 1 mW.

**S1.2. Reduced graphene oxide film enhances the F-SBS**

Graphene enhances the F-SBS via influencing the $g_B$ and the $L_{\text{eff}}$ of the pump mode majorly. Here $L_{\text{eff}}$ relates to the loss while $g_B$ is determined by the material,

$$g_B \propto \frac{4\pi^2 \gamma_e^2}{n_p c \lambda_p^2 \rho_0 v_A \Gamma_B}$$

(S6)

Here $\gamma_e$ is the electrostrictive coefficient, $n_p$ is the effective index of the pump mode, $\Gamma_B$ is the lifespan of the phonons. Determined by its permittivity, the rGO film has high optical index: $n_{rGO}$ is higher than 3 in C-band [S2,S3]. As a result, at the same frequency, $n_p$ of a specific pump mode in the graphene based WGM cavity is smaller than the one in the silica cavity, and high order modes are enhanced, hence $L_{\text{eff}}$ of high order modes increase. Moreover, rGO brings a much higher $\gamma_e$ than silica [S4], consequently, $g_B$ could be enhanced in the rGO based WGM cavity.
S1.3. Gas adsorption based phonon excitation

In the GBMR, gas detection relies on the phase matching of the optomechanical modes. Spectral shift of the \( f_s \) is determined by the \( \nu_A \) majorly:

\[
\frac{\partial f_s}{\partial x} = \frac{2\pi n_s - 2\pi n_p}{(c - 2\pi \nu_A n_s)} \frac{\partial \nu_A}{\partial x} f_p \tag{S7}
\]

Here \( x \) is the gas concentration, \( n_s < n_p \), and we approximately assume the change of the \( n_s \) is negligible. This equation reveals that when \( \nu_A \) decreases with gas concentration, \( f_s \) increases accordingly, which also verifies that \( f_M = f_p - f_s \) decreases when launching a higher gas concentration. In terms of the \( \nu_A \), it obeys the media equation \( \nu_A = (E_Y/\rho)^{1/2} \), wherein \( E_Y \) is the elastic modulus of the cavity, and \( \rho \) is the density. According to previous researches, gas adsorption induced surface defect in the rGO film reduces the \( E_Y \). Figure S2 plots the theoretically calculated results. With gas concentration increasing, graphene’s elastic modulus decreases from \( \approx 1.15 \) TPa to 1.09 TPa, while the effective acoustic velocity of the graphene-silica cavity decreases from \( \approx 5660 \) m/s to 5480 m/s. In our GBMR, the effective inner surface area deposited by rGO is \( 2.6 \times 10^{-2} \) mm\(^2\), the number of NH\(_3\) gas molecules adsorbed on the is on \( 10^{11} \) level.

Fig. S2. Calculated results of the elastic modulus of the rGO (blue solid curve), and the acoustic velocity of the cavity (red dashed curve).

S2. Fabrication of the graphene enhanced Brillouin microresonator (GBMR)

Fabrication process of the GBMR for WGM resonance is shown in Figure S3a. First, commercial silica capillary (CV17-100) with 100 µm outer diameter and 17 µm thick wall
was fixed in a programmable fiber splicer (Fusion FITEL-S184, JPN). By setting parameter ‘150 mA/200 ms + 200mA / 100 ms’, we heated the capillary via arc discharge. Due to thermal expansion of the internal air, fused silica capillary was reformed to be a Bottle cavity. The fabricated Bottle cavity has a diameter of 118 µm and a minimum wall thickness of 8 µm. Then it was washed by alcohol and DI water.

1 mg Graphene oxide powder was dissolved in 100mL DI water with sonication for 2 hours to form a uniform dispersion. Then the GO dispersion was injected into the capillary via fluidic tube. After 24 hours, the water of the GO dispersion was evaporated naturally in air at room temperature, therefore the thin GO film was deposited on the inner wall of the Bottle cavity. Afterwards we injected hot Vitamin C aqueous solution (20g/L) in the capillary, keeping the GO film reduced by the Vitamin C solution (40 °C) for 1.5 hour. Then the GO film was reduced to be a thin rGO film. Finally, the rGO based capillary was washed by DI water for several times and gently dried on a heat-port. We also described this technique in Ref. (29). It is worth noting that to ensure the rGO film uniform and thin (to avoid too much loss), solution concentration should be low and the reduction process should be controlled slow. Figure S3b and S3c shows the X-ray photoelectron spectra (XPS) of the GO film and the rGO film, respectively. Compared to the GO film, the rGO film has ≈ 2 times higher C:O ratio, implying that the reduction is effective.
**Fig. S3. Fabrication of the GBMR.** a, The silica bottle cavity was bubbled by a fiber splicer, and then rGO film was deposited in its inner wall via Vitamin C reduction. b, XPS of the GO film, c, XPS of the rGO film.

**S3. Measuring optical Q factors of the WGM resonators**

Figure S4c plots the measured $Q$ factors of the 3 types for fundamental mode resonances around 1550 nm: Determined by the dimensional restrictions, the cylindrical capillary has a typical $Q$ factor is $\approx 10^6$; the bottle-shaped capillary can have a much higher $Q$ factor approaching $8\times 10^6$; and the microsphere has the highest $Q$ factor $> 1.4\times 10^7$. However, gas flow cannot pass through the microsphere. Hence, the bottle-shaped capillary with both a through channel for gas flow and a relatively high $Q$ factor is adopted in this work. Figure S4d provide two more resonance dip examples of the bottle-shaped cavity, with central wavelength at 1534.7 nm (fundamental mode, $Q \approx 8\times 10^6$) and 1592.3 nm (fundamental mode, $Q \approx 7\times 10^6$). Figure S4e provide two more resonance dip examples of the GBMR.
cavity, with central wavelength at 1534.6 nm (fundamental mode, $Q \approx 2 \times 10^6$) and 1594.1 nm (fundamental mode, $Q \approx 1.8 \times 10^6$). For wavelength in range of 1530 nm to 1570 nm, the $Q$ factor of the fundamental mode in the bottle-shaped cavity keeps $\approx 8 \times 10^6$, and the $Q$ factor of the fundamental mode in the GBMR cavity keeps $\approx 2 \times 10^6$. For lower optical frequencies (> 1580 nm), due to scattering based loss, the $Q$ factor would be a bit lower.

**Fig. S4. Measurement of the transmissions and optical $Q$ factors.**

- **a**, Experimental setup.
- **b**, Three different WGM resonators.
- **c**, Optical $Q$ factor of the resonators for fundamental mode at wavelength $\approx 1552$ nm.
- **d**, Two examples of resonance dips of the bottle-shaped WGM microresonator.
- **e**, Two examples of resonance dips of the GBMR.
S4. Experimental setup and preparation of the gas samples

Figure S5 shows the experimental setup to generate the F-SBS and detect the gas concentration. A tunable laser (Agilent B1636B, USA, resolution 1 pm) works as the pump, which is carefully tuned in the resonances to find the F-SBS. A fiber polarization controller (FPC) is used to control the coupling modes. Collected light from the WGM cavity is launched in a photodetector (Thorlabs, USA, 1.25GHz) and a high resolution OSA (APEX AP2051A, France, resolution 0.02 pm), via an optical fiber coupler. The beat note is monitored by a RF spectroscope (Agilent N9020A, USA). In experiment, we carefully tune the pump frequency to find phase-matched point, in span of 1520 nm to 1590 nm, by monitoring the beat note on RF spectroscope. Considering the generated F-SBS intensity, SNR, frequency, and stability together, we select the mechanical mode in order of 24 ($f_M = 262$ MHz) for gas detection. In gas detection, the pump frequency and polarization is fixed.

Fig. S5. Experimental setup. Red path: optical fibers, black path: electronics, Yellow arrows: gas direction. FPC: fiber polarization controller, PD: photodetector.

Figure S6 shows the process we prepare NH$_3$ gas samples with concentration of 1 ppm to 20 ppm. First, pure NH$_3$ gas (100% concentration) is drawn out from the gas chamber, by using micro syringe. The volume is controlled as 1 µL, 2 µL, 3 µL, 4 µL, 5 µL, 10 µL, and 20 µL, respectively. Then the pure NH$_3$ gas is injected another gas buffer, whose
volume is 1 L. Hence we get NH₃ samples with concentration of 1 ppm to 20 ppm. Finally the samples with certain concentration is injected into the GBMR.

![Preparing the gas samples](image)

**Fig. S6. Preparing the gas samples.** By using micro syringe, pure NH₃ gas is diluted to be 1 ppm ~ 20 ppm and then launched into the GBMR.

**S5. Gas detection experiment based on BMR without rGO film deposition**

BMR without graphene material can support resonant multimodes and F-SBS generation as well. Figure S7 maps the spectrum of a mechanical mode (We select a mode with similar order to the one in the GBMR) generated in a BMR, varying with NH₃ gas concentration change. Because there is no material to adsorbing the gas molecules, the beat note cannot shift obviously, obeying the fixed phase-matching condition. Related to previously reported µFOM structure measuring liquid [S5], NH₃ gas cannot affect the silica cavity so much.

![Spectral response of the BMR](image)

**Fig. S7. Spectral response of the BMR.** By increasing the NH₃ gas concentration, there is no obvious change on the spectra.
S6. Instability of the GBMR

Figure S8a and S8b show the measured power instability and the spectral uncertainty of the mechanical resonance (Mode 24 at 262 MHz) during gas detection, respectively. At each gas concentration, we sample 10 points (1 point per second). As Figure S8a plots, amplitude instability of the GBMR is ≈8 dB, which is influenced by the thermal noise, the Brillouin gain, the detuning, and the PD accuracy, etc. Fortunately, SNR of the beat note keeps > 30 dB, the spectral location of the beat note could still be extract in high resolution. Corresponding to the main text, Figure S8b plots the uncertainty of the beat note spectrally. It varies in hundreds Hz. A higher gas concentration tends to bring stronger instability.

![Fig. S8. Uncertainty of the resonant mode in the GBMR. a, power instability. b, Spectral instability. In a, the dashed lines show the average edge of the power instability, in b, the dashed line shows the central frequency.](image)

S7. Supplementary discussion about the performances

Table S1 concludes the comparison of the performances of recent gas sensors. Related of the state-of-literature optical gas sensors, this work shows unique advantages. *NG means Not Given.
Table. Comparison of state-of-art optical gas sensors

<table>
<thead>
<tr>
<th>Sensor type</th>
<th>Detect limit</th>
<th>Dynamic range</th>
<th>Response speed</th>
<th>Compactness</th>
<th>Reference</th>
</tr>
</thead>
<tbody>
<tr>
<td>Photothermal spectroscopy</td>
<td>2 ppb</td>
<td>6 orders</td>
<td>minutes</td>
<td>meters long</td>
<td>S6</td>
</tr>
<tr>
<td>Graphene based optical interferences</td>
<td>sub ppm</td>
<td>2 orders in average</td>
<td>seconds</td>
<td>cm level</td>
<td>S7</td>
</tr>
<tr>
<td>Graphene based SPR</td>
<td>1 ppm</td>
<td>NG</td>
<td>minutes</td>
<td>NG</td>
<td>S8</td>
</tr>
<tr>
<td>Ultrasensitive plasmonic sensors</td>
<td>~ ppm</td>
<td>NG</td>
<td>NG</td>
<td>tens of cm</td>
<td>S9</td>
</tr>
<tr>
<td>Visible spectroscopy</td>
<td>5 ppb</td>
<td>NG</td>
<td>minutes</td>
<td>NG</td>
<td>S10</td>
</tr>
<tr>
<td><strong>Graphene enhanced SBS</strong></td>
<td><strong>1 ppb</strong></td>
<td><strong>5 orders</strong></td>
<td><strong>seconds</strong></td>
<td>&lt;cm</td>
<td><strong>This work</strong>*</td>
</tr>
</tbody>
</table>

**Supplementary References**


